SULFUR DIOXIDE GAS ADSORPTION STUDY USING MIXED ACTIVATED CARBON FROM DIFFERENT BIOMASS

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ABSTRACT

Activated carbon produced from coconut shell and rubber seed pericarp has a great potential to be used as gas adsorbent. Most researchers, however, focus on producing activated carbon from one single biomass. Another option is to produce activated carbon from blending two different types of biomass with the strategy to reduce dependency on one type of biomass and sustain the production of activated carbon. Further, the adsorption capacity of the activated carbon produced from different blended biomass would be increased in comparison to single biomass. Most activated carbon is produced via physical activation using the conventional pyrolysis heating system, which is very time-consuming. In this study, activated carbon from biomass, namely coconut shell (CS-AC), rubber seed pericarp (RSP-AC), and their blends (CSRSP-AC) were successfully produced by using ZnCl₂ as the chemical activating agent. The activation process was performed in a modified commercial microwave oven at the irradiation power of 600 W for 20 min. The single activated carbon and its blend were tested for their adsorption capacity for sulfur dioxide gas (SO₂) using evolved gas analyzer (EGA). The single RSP-AC and CS-AC samples produced breakthrough time for SO₂ adsorption at 23 min and 14 min, respectively. The longest SO₂ breakthrough time for the blended activated carbon (CSRSP-AC) was achieved at 15 min with a ratio of 20:80 (CS:RSP) and was slightly longer than the individual CS-AC. The high amount of microporous RSP in the blend increases SO₂ adsorption capacity. The presence of fly ash/Ca(OH)₂ catalyst in the blended CSRSP-AC (20:80) further improves SO₂ adsorption capacity with the breakthrough time achieving at 36 min at the adsorption temperature of 35°C. The SEM micrograph of blended CSRSP-AC with the addition of fly ash/Ca(OH)₂ catalyst after SO₂ adsorption showed that the pores were clogged with some of the samples agglomerated and clustered, indicating that both activated carbon and fly ash/Ca(OH)₂ catalyst had interacted thoroughly with SO₂ after the adsorption process.

Keywords: Activated carbon; Coconut shell; Gas adsorbent; Microwave; Rubber seed pericarp; Sulfur dioxide

1. INTRODUCTION

One of the emissions polluting the atmosphere is sulfur dioxide (SO_2) , which is mainly released by industries threatening the environment and human health (Uçar et al.,

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2009; Sumathi et al., 2010). The elimination of this gas from the stationary sources is important to prevent it from polluting the environment. Recently, many researchers have studied the removal of SO_2 gas by using carbon-based materials (Bai et al., 2016; Sun et al., 2018; Shao et al., 2018).

In Malaysia, a high capacity of electricity is generated through the thermal power plants where the main source of fuel is supplied by burning coal. In recent years, about 2420 MW of electricity has been generated from Sultan Salahuddin Abdul Aziz Shah power station, Kapar, Selangor by using more than a hundred tons of coal for the national usage (Amin et al., 2013). However, an increase in Malaysia's coal power plants leads to an increase in the formation of fly ash, which is a residue formed as a result of the combustion of bituminous coal (Ismail et al., 2007). This fly ash has a glassy, spherical shape with a very fine structure similar to that of cement. According to Wang and Wu (2006), the presence of fly ash has posed the industry the challenge of disposing and creating a more efficient recycling technique.

This work has studied the adsorption of SO₂ on activated carbon, prepared from the coconut shell, rubber seed pericarp, and their blends. Activated carbon was prepared using the microwave irradiation technique. Previous researchers have reported the use of microwave heating in pyrolyzing the crude oil and other carbon materials (Leong et al., 2016; Yang & Ani, 2016). This study provides comprehensive data about the cleaning of SO₂ gas by using activated carbon from blending the coconut shell and rubber seed pericarp. The blended activated carbon was utilized in the presence of coal fly ash to improve the efficiency of SO₂ adsorption. The coconut shell and rubber seed pericarp have successfully been converted into well-developed activated carbon with microporous characteristics and used to adsorb SO₂ (Shukor et al., 2017). The effect of four important parameters have been investigated, and these include the blending ratio of activated carbon (CS:RSP), mass loading of sample in combustion cell, adsorption temperature, and addition of fly ash/Ca(OH)₂ toward SO₂ adsorption. These parameters were chosen for investigation because of their significant influence on SO₂ adsorption (Sumathi et al., 2010; Rubio & Isquierdo, 2010). Further, the surface morphology of adsorbent before and after adsorption was also carried out to understand the effect between surface chemistry of adsorbents on the adsorption process.

2. METHODS

2.1. Sample Preparation

CS-AC, RSP-AC, and CSRSP-AC used in this study were prepared by chemical activation using $ZnCl_2$ as the activating agent. The details of the preparation method have been reported elsewhere (Shukor et al., 2017). The weight sample (10.00±0.01 g) of the coconut shell, the rubber seed pericarp, and their blends (0:100, 20:80, 50:50, 80:20, and 100:0 (%w/w)) were added to 50% of ZnCl₂ solutions in a ratio of 1.5 g/g sample at room temperature for 24 hr. The impregnated sample was heated using microwave irradiation at 600 W in the presence of nitrogen gas for 20 min (Idris et al., 2012). Then, the sample was washed with 0.1M HCI and with cold distilled water to remove the organic matter residues until it was neutralized until pH 7. Finally, the sample was dried in an oven at 100°C overnight and ready for further analysis.

2.2. Catalytic Sorbent Preparation

The catalytic sorbent was prepared by using the impregnation method. The coal fly ash was mixed with $Ca(OH)_2$ and activated carbon (AC) in the presence of water in 1:1:1 (%w/w) ratio. The entire slurry sample formed was stirred and heated to 90°C for 48 hr. The sample was cooled and kept in a glass desiccator for further analysis.

2.3. Sample Characterization

The surface area of the sorbent was determined by N_2 adsorption of Brunauer-Emmet-Teller (BET) using Model TM-3030Plus Tabletop Microscope. The BET surface area was measured by means of standard BET equation, applied with relative pressure (P/P₀) ranging from 0.01 to 0.90. The samples for the SEM analysis were prepared by cutting and placing the dried samples on a carbon tape to fit the specimen stub before being viewed.

2.4. Activity Test

The SO₂ absorption activity test was performed using a fabricated fixed bed combustion cell (see Figure 1). The standard SO₂ gas was measured and analyzed using an evolved gas analyzer (EGA) (Siemens Ultramat-23). About 1.0 g to 5.0 g of sample (i.e., single and blended activated adsorbent with and without fly ash/Ca(OH)₂ was dispersed on 0.05 g borosilicate glass wool located at the center of the combustion cell. Then, SO₂ gas at the initial concentration of 1000 ppm with N₂ as balanced at the flow rate of 500 ml min⁻¹ was passed through the sample at different temperatures ranging from 35°C to 200°C. The concentration of SO₂ gas before and after sorption process was measured and recorded continuously for every minute until it reached the breakthrough point (C/C₀ versus time). The amount of SO₂ gas adsorbed by the sorbent was evaluated as adsorption breakthrough time of SO₂ until both the inlet and outlet SO₂ concentration became the same (Dahlan et al., 2008; Sumathi et al., 2010).



Figure 1 Schematic flow diagram of the evolved gas analysis experimental set-up for SO₂ absorption activity test

3. RESULTS AND DISCUSSION

3.1. Fly Ash Composition

The results of XRF on the coal fly ash is shown in Table 1. The major composition of metal oxides present are SiO₂, followed by Al₂O₃, Fe₂O₃, TiO₂, CaO, K₂O, P₂O₅, and MgO at the percentages of 59.4%, 21.6%, 9.19%, 3.22%, 2.78%, 1.51%, 0.86, and 2.78%, respectively. The other metal oxides and traces compound with minor composition of less than 1% are also presented in Table 1. According to Yao et al. (2015), coal fly ash could be used as support catalyst for various reactions, due to the higher stability of its principal component of metal oxides present in it. Fly ash that consists of higher content of oxides, such as iron oxides, poses a higher thermal stability, which can be utilized in heterogeneous catalyses. Moreover, Wang (2008) has reported that fly ash is effective to be used as catalyst for various reactions, such as solid, liquid, and gas phase oxidation.

Element	$\% M_X O_Y$	
SiO ₂	59.40	
Al_2O_3	21.60	
Fe ₂ O ₃	9.19	
TiO ₂	3.22	
CaO	2.78	
K ₂ O	1.51	
P_2O_5	0.86	
MgO	0.30	
Traces Element	<1	

Table 1 The element composition of metal oxides present in fly ash

3.2. SO₂ Adsorption Activity Test

The SO₂ adsorption activity test is reported as the breakthrough time curve (C/C_o versus t), where C_o is the initial concentration of SO₂ (ppm) passing through the adsorbent, while C is the outlet concentration of SO₂ (ppm) recorded from the gas analyzer. The effect of the activated biomass blending ratio was studied and the best adsorption breakthrough time of the blended sample was selected to further study its effect on other parameters, namely the amount of mass load in the combustion cell, the adsorption temperature, and the addition of catalytic fly ash/ Ca(OH)₂ on the selected blended sample.

3.2.1. Effect of activated biomass blending ratio on SO₂ breakthrough time curve

The effect of the blending ratio of activated biomass was investigated based on the breakthrough time curve. According to Sumathi et al. (2010), the sample is considered a good sorbent when it can maintain longer breakthrough time for 100% adsorption of SO₂. Figure 2 shows the breakthrough time curve of the blended sample at different ratios of 100:0 (CS:RSP), 80:20 (CS:RSP), 50:50 (CS:RSP), 20:80 (CS:RSP), and 0:100 (CS:RSP), and the SO₂ breakthrough times are portrayed in Table 2.



Figure 2 SO₂ adsorption breakthrough time curves for single (CS-AC and RSP-AC) and blended CSRSP-AC at 50% of ZnCl₂ concentration with impregnation ratio of 1.5 at 35°C

Table 2 SO₂ adsorption breakthrough time of 1.0 g single and different blended sample ratios

Blended sample (CS:RSP)	Adsorption breakthrough time (min)
100:0	14
80:20	6
50:50	8
20:80	15
0:100	23

The results in Table 2 illustrate that single RSP-AC exhibits the longest adsorption breakthrough time of 23 min in comparison to the other blended sample at adsorption temperature of 35°C. Similarly, the single CS-AC exhibits adsorption breakthrough time of 14 min. Apparently, the blended adsorbent with ratio of 20:80 (CS:RSP) exhibits the longest breakthrough time of 15 min in comparison to 80:20 (CS:RSP) and 50:50 (CS:RSP) at 6 min and 8 min, respectively. This observation indicates that a high ratio of RSP over CS in the blend promotes a larger adsorption capacity for SO₂. Liu and Adanur (2014) have reported that the higher micropore present in the adsorbent increases the capability of SO₂ absorption because mesopores and macropores encourage the blockage of the surface adsorbent. In other words, the SO_2 breakthrough time of adsorbent is directly dependent on the ratio of micropore present in the sample. The blended activated sample of 80:20 (CS:RSP), consisting of mainly mesopores, exhibits the lowest breakthrough time of 6 min due to the higher ratio of CS over RSP. This blended sample rapidly became saturated by SO₂ after the breakthrough and produced a steeper slope in the curve. Similarly, the 50:50 (CS:RSP) blended sample also has a shorter breakthrough time with steeper slope, which reflects a lower adsorption capacity due to the poor development of porous structure (Izquierdo & Rubio, 2008). Hence, the adsorbent with a blending ratio of (20:80) exhibits a higher adsorption capacity in comparison to the other blending ratio and was selected to observe the effect of other parameters affecting the SO_2 adsorption breakthrough time.

3.2.2. Effect of adsorbent mass load in the combustion cell on SO_2 breakthrough time curve Figure 3 shows the effect of mass sample loading in the fixed bed combustion cell. The blended activated sample with a ratio of 20:80 (CS:RSP) ranging from 1.0 g to 5.0 g was analyzed for the SO_2 adsorption capacity test. The SO_2 adsorption breakthrough time at different mass loading of adsorbents are tabulated in Table 3.



Figure 3 SO₂ adsorption breakthrough time curves for CSRSP-AC (20:80) at different mass loading in combustion cell at 35°C

Table 3 Comparison of adsorption breakthrough time from different mass of sample

Adsorbent mass (g)	Adsorption breakthrough time (min)		
1.0 g sample	15		
2.0 g sample	16		
3.0 g sample	20		
4.0 g sample	26		
5.0 g sample	29		

Apparently, the 1.0 g of blended sample showed the lowest breakthrough time of 15 min followed by 2.0 g, 3.0 g, 4.0 g, and 5.0 g at 16 min, 20 min, and 29 min of front time, respectively, for which an increment of SO₂ breakthrough time was observed. The lower adsorbent mass loading in the combustion cell causes the sample to become rapidly saturated after breakthrough. Increasing the mass load of adsorbent in the cell slightly increases the breakthrough time of SO₂ adsorption. The lower mass of sample loaded in the cell generates steeper gradient of the curve, which indicates that SO₂ adsorption is less effective in comparison to high mass loading. Moreover, the 5 g sample is considered the maximum limit, due to the limitation of the sample cup size used in the combustion cell. Hence, 5.0 g of blended CSRSP-AC (20:80) were found to achieve the longest SO₂ adsorption breakthrough time.

3.2.3. Effect of adsorption temperature on SO₂ *adsorption breakthrough time curve*

One of the important factors affecting the performance of SO_2 adsorption capacity is the gas absorption temperature. Figure 4 shows the results of breakthrough time of the activated sample subjected to SO_2 gas adsorption ranging from 35°C to 200°C (also see Table 4 for a summary).



Figure 4 SO₂ adsorption breakthrough time curves for 5.0 g of blended adsorbent CSRSP-AC (20:80) at different adsorption temperatures

Table 4 SO₂ adsorption breakthrough time at different gas adsorption temperatures

Gas Adsorption Temperature (°C)	Adsorption breakthrough time (min)	
35	29	
100	24	
150	22	
200	14	

The SO₂ adsorption breakthrough time slightly decreased with the increasing temperature. At a high temperature, the kinetic energy of SO₂ molecules decreased, causing the adsorption process to become exothermic (Karatepe et al., 2008). Moreover, according to Wang et al. (2016), the process of gas adsorption molecule normally undergoes exothermic reaction, in which the adsorption process decreases with an increasing temperature. As shown in Figure 4, SO₂ adsorption capacity was inhibited by the increasing temperature from 100°C to 200°C. Hence, the lower the adsorption temperature was, the greater the SO₂ breakthrough time was recorded. Apparently, the SO₂ adsorption improved at the reaction temperature of 35°C. The longest SO₂ breakthrough time of 29 min was observed at the temperature of 200°C at 14 min, followed by 150°C and 100°C at 22 min and 24 min, respectively. The reduction of SO₂

adsorption capacity at the same time as the increase in reaction temperature is due to the saturation of carbon surface of the activated sample. The active sites of the surface sample are blocked by sulfur and can be seen by the breakthrough profile (see Figure 4), where much steeper slopes were observed at a high temperature. At a lower temperature, the physical adsorption can be controlled, where the process undergoes catalytic oxidation in which SO₂ is oxidized to SO₃ by O₂ and assumed as the controlling step (Wang et al., 2016). The physical adsorption at the sample surface, however, is inhibited at a high temperature, causing a small amount of SO₂ being oxidized. Thus, the performance of SO₂ adsorption capacity is reduced as the temperature increases. A similar observation was reported by Lee et al. (2002) with a biomass sample impregnated with KOH, where adsorption capacity decreased as the temperature increased. This result is consistent with SEM micrograph and BET data.

3.2.4. Effect of fly ash on SO_2 adsorption breakthrough time curve

The SO₂ adsorption breakthrough time curve of blended adsorbent CSRSP-AC (20:80) with and without the presence of mixed fly ash/Ca(OH)₂ is shown in Figure 5 and summarized in Table 5. The results in Figure 5 indicate that the addition of fly $ash/Ca(OH)_2$ promotes a better performance of the SO₂ adsorption breakthrough time, reaching up to 36 min with a lower slope increase on the curves. It can be seen that both CSRSP-AC (20:80) sample and a mixture of CSRSP-AC (20:80) with fly ash/Ca(OH)₂ demonstrated a sharp increase before subsequently achieving complete saturation after 260 min. The coal fly ash consists of mainly silica and alumina with some metal oxides, namely Fe₂O₃, CaO, and MgO (see Table 1). In addition, the fly ash also poses large surface area of 40 to 115 m^2/g . When siliceous material, such as fly ash, is mixed with Ca(OH)₂ in hydration process, the pozzolanic reaction between alumina and silica are eluted from fly ash and calcium hydroxide. The reaction species of a complex compound was formed where the adsorbent with a high surface area and SO₂ capture activity could be obtained (Jain et al., 2011). Previously, Zainudin et al. (2005) had reported that BET surface area of calcium hydroxide was 6.18 m²/g. This shows that calcium hydroxide has a porous structure too. This characteristic gives advantage to both fly ash and calcium hydroxide as adsorptive materials. Therefore, the mixture of calcium hydroxide as support material on fly ash and mixed adsorbent improved the SO₂ adsorption breakthrough time. Further, the presence of Fe₂O₃ in the fly ash also catalyzed the oxidative reaction of SO₂ to SO₃ (Belo et al., 2014). The SO₃ is easily captured by CaO and MgO in the fly ash forming sulfates, which leads to a higher removal of SO₂ from the system, as indicated by longer breakthrough time (Wang et al., 2012).



Figure 5 SO₂ adsorption breakthrough time for 5.0 g of blended CSRSP-AC (20:80) at 35°C adsorption temperature with and without fly $ash/Ca(OH)_2$

Sample	Time (min)	
CSRSP-AC (20:80) at 25°C	29	
Fly ash + Ca(OH) ₂ at 25° C	16	
CSRSP-AC (20:80) + Fly ash + Ca(OH) ₂ at 25° C	36	

Table 5 Comparison of adsorption breakthrough time of CSRSP-AC (80:20) with and without fly ash/Ca(OH)₂ as catalyst

3.3. Comparison of SEM Image

Figure 6 compares the surface morphology of the samples before and after SO₂ adsorption based on the effect of temperature and catalyst. Figure 6a corresponds to CSRSP-AC with a ratio of 20:80 (CS:RSP) before the SO₂ adsorption process. The micrograph shows the presence of pores on the surface of the sample. Figure 6b shows the micrograph of CSRSP-AC with the ratio of 20:80 (CS:RSP) after SO₂ adsorption at 35°C. Apparently, the porous surface of the adsorbent was less visible and clogged up after the reaction with SO₂. These observations are almost similar to SEM micrograph reported by Zainudin et al. (2005) before and after the SO₂ capture. At 100°C, the surface of the sorbent (see Figure 6c) is thick, and the pores are no longer visible because they are covered by a layer of product (sulfate) after the adsorption of SO_2 . This means that the SO_2 contaminants are fully adsorbed by the sorbent after the SO_2 adsorption process. The pore structures get blocked as the temperature increases and this causes a decrease in the breakthrough time of SO_2 gas adsorption. Figure 6d shows the surface morphology of CSRSP-AC (20:80), coated with fly ash/Ca(OH)₂ after the SO₂ adsorption. The sample surface was clogged, and some of the ash spherical structure was deposited on the sample surface. These images are also consistent with the breakthrough time of SO₂ gas adsorption in which the extra fly ash improves the SO₂ adsorption performance. Figure 6e illustrates the SEM micrograph of fly ash/Ca(OH)₂ after SO₂ adsorption. The surface was covered by lumps, and some agglomerates were clustered on the plate, illustrating that the SO₂ was adsorbed thoroughly by fly ash/Ca(OH)₂.



Figure 6 SEM image (1000×) of: (a) CSRSP-AC (20:80) before adsorption; (b) CSRSP-AC (20:80) after SO₂ adsorption at 35°C; (c) CSRSP-AC (20:80) after SO₂ adsorption at 100°C; (d) CSRSP-AC (20:80) coated with fly ash and Ca(OH)₂ after SO₂ adsorption; (e) fly ash and Ca(OH)₂ after adsorption of SO₂

3.4. The BET Surface Area

Table 6 shows the BET surface area of the blended CSRSP-AC with a ratio of 20:80 (CS:RSP) before and after SO₂ adsorption at the temperatures of 35°C and 100°C. The blended sample before adsorption exhibits a higher BET surface area of 332.83 m²/g with a total pore volume of 0.14702 cm³/g and a pore diameter of 2.8501. A high BET value was detected because the sample was not subjected to SO₂ adsorption. This conforms to the SEM image (Figure 6a), which displays well-developed pores drilling over the surface of the adsorbent. However, the BET value dropped after the adsorption of SO₂ at 35°C with 295.63 m²/g of BET surface area, 0.12853 total pore volume, and 2.7143 nm of pore diameter. This indicates that the blocking of some pores and the adsorption of SO₂ on the surface of the adsorbent were successful since the

BET value declined. According to Liu and Adanur (2014), the adsorption capacity of gases are inversely proportional to pore size and pore volume where adsorbates with smaller pores are better able to adsorb the gas contaminant. It is noticeable that increasing the SO₂ absorption temperature from 35° C to 100° C will slightly increase the BET surface area of the adsorbent. In addition, the total pore volume (V_{tot}) also increases in the same manner as the BET surface area with a value of 0.13178 cm^3 /g. It seems that the adsorbent becomes slightly porous after the SO₂ adsorption, indicating that less pore blockage has occurred. However, the difference between the BET surface area and the total pore volume between the blended samples after SO₂ treatment at 35°C and 100°C are considered small. To verify further, these selected adsorbents were subjected to the SEM analysis to observe the surface morphology after 35° C and 100° C SO₂ adsorption treatment. The SEM images of both samples (see Figure 6) illustrated the thickening of the adsorbent wall with the appearance of lumps (i.e., sulfated products) as a result of SO₂ absorption reaction.

Table 6 Pore characteristics of CSRSP-AC adsorbent (20:80; CS:RSP) before and after SO₂ gas adsorption at different adsorption temperatures

Sample	$S_{BET} (m^2/g)$	V_{Tot} (cm ³ /g)	D _p (nm)
CSRSP-AC before adsorption	332.83	0.14702	2.8501
CSRSP-AC after SO ₂ adsorption at 35°C	295.63	0.12853	2.7143
CSRSP-AC after SO ₂ adsorption at 100°C	296.52	0.13178	3.2205

 S_{BET} : BET surface area; V_{Tot} : Total pore volume; D_p : Average pore diameter

4. CONCLUSION

Adsorption capacity of SO₂ on biomass activated carbon (CS-AC, RSP-AC) and their blends (CSRSP-AC) were tested and monitored by an evolved gas analyzer. The single microporous RSP-AC exhibits the longest SO₂ breakthrough time of 23 min in comparison to the single CS-AC at 14 min. Among the blended samples, the 20:80 (CS:RSP-AC) was found to have the longest SO₂ adsorption breakthrough time (C/C_o) of 15 min. A high amount of RSP in the blended sample promotes a longer SO₂ breakthrough time. The relationship between the SO₂ breakthrough time recorded was at 35°C with 29 min of adsorption breakthrough time. Increasing the adsorption temperature slightly reduces the SO₂ adsorption capacity. The addition of fly ash/Ca(OH)₂ catalyst that contains CaO and MgO with activated carbon increases the performance of adsorption capacity, where the breakthrough time was increased to 36 min. The SEM image showed that the porosity of adsorbent was reduced through the surface coverage by the reaction of the product, which means that the SO₂ adsorption activity has been successful.

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